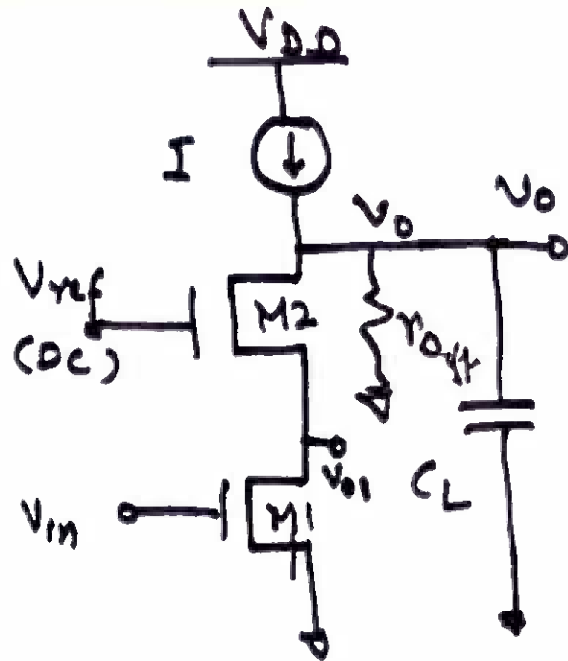


Cascode Amplifier



M_1 & M_2 are so biased with current source I , such that they remain in saturation.

M_2 is further applied a DC voltage V_{ref} . However Gate of M_2 is at '0' volt for AC operation.

M_1 is the Driver Transistor

C_L is capacitive Load.

The output resistance of Current Source is v. high $\rightarrow \infty$



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We wish to find $g_{m\text{eff}}$ and $g_{o\text{eff}}$ of this cascode stage.

Let g_{m1} and g_{o1} ($\frac{1}{r_{o1}}$) are the transconductance and output conductance of Transistor $M1$ &

Similarly g_{m2} & g_{o2} are for Transistor $M2$

By network theorems small signal current i (dI) is given by

$$i = g_{m\text{eff}} \cdot v_{in} + g_{o\text{eff}} v_o \quad \text{--- (1)}$$

Let v_{o1} be drain voltage of $M1$. However this voltage is also 'Source' voltage of $M2$.



For AC signal, $V_{GS_2} = 0 - v_{o1} = -v_{o1}$

From current equation ①

$$g_{m_{eff}} = \left. \frac{i}{v_{in}} \right|_{v_o = 0} \quad \text{and} \quad g_{o_{eff}} = \left. \frac{i}{v_o} \right|_{v_{in} = 0}$$

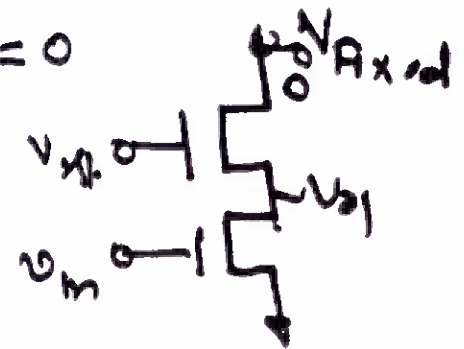
Assume we apply a fixed voltage V_{FIX} at the Drain of M_2 (v_o terminal). Then for ac case, $v_o = 0$

$$\therefore (v_o - v_s)_{M_2} = v_{GS_2} = -v_{o1}$$

Then

$$\therefore i = g_{m_1} v_{in} + g_{o_1} (+v_{o1}) \quad \text{--- ②}$$

$$\& i = g_{m_2} (-v_{o1}) + g_{o_2} (-v_{o1}) \quad \text{--- ③}$$





From eq (3) $v_{o1} = \frac{-i}{g_{m2} + g_{o2}}$

substituting this in eq (2) as

$$i = g_{m1} v_{in} + \frac{-g_{o1} i}{g_{m2} + g_{o2}}$$

$$\therefore i \left(1 + \frac{g_{o1}}{g_{m2} + g_{o2}} \right) = g_{m1} v_{in}$$

$$\therefore g_{meff} = \frac{i}{v_{in}} = \frac{g_{m1}}{\left(1 + \frac{g_{o1}}{g_{m2} + g_{o2}} \right)}$$



$$\text{OR } g_{m\text{eff}} = \frac{g_{m1} (g_{m2} + g_{o2})}{g_{m2} + g_{o1} + g_{o2}}$$

If r_o of $M1$ & $M2$ are large, then g_{o1} & g_{o2} are very small.

$$\therefore g_{m\text{eff}} \approx \frac{g_{m1} g_{m2}}{g_{m2}} \approx g_{m1}$$

Hence we observe that $g_{m\text{eff}}$ of the Cascode Stage is almost same as g_{m1} .

→ Hence if we have normal amplifier without $M2$, then Transconduct. $g_m = g_{m1}$

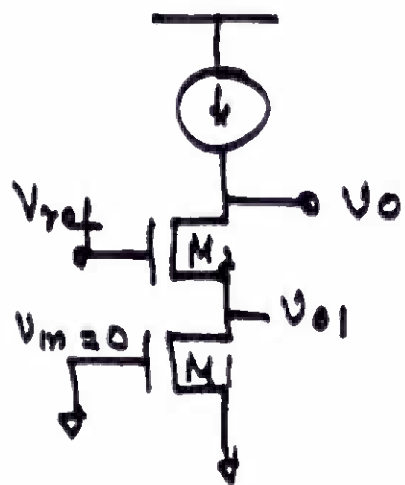


Next we evaluate g_{eff} .

To get g_{eff} , from equ. (1) we have

$$g_{\text{eff}} = \frac{i}{v_o} \Big|_{v_{\text{in}} = 0}$$

\therefore Circuit looks like as shown in Fig. We do ac analysis and get



$$i = -g_{m2} v_{o1} + g_{o2} (v_{o2} - v_{o1}) \quad \text{--- (4)} \quad v_o = v_{o2}$$

$$\therefore i = g_{m1} \cdot 0 + g_{o1} v_{o1} \quad \text{--- (5)}$$

$$\therefore v_{o1} = \frac{i}{g_{o1}}$$

Substituting this in eq (4)

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$$\therefore i = -\frac{g_{m2}i}{g_{o1}} + g_{o2}V_o + g_{o2}\left(-\frac{i}{g_{o1}}\right)$$

$$\text{or } i\left(1 + \frac{g_{o2}}{g_{o1}}\right) + \frac{(g_{m2})i}{g_{o1}} = g_{o2}V_o$$

$$\therefore g_{o\text{eff}} = \frac{i}{V_o} = \frac{g_{o2}}{1 + \frac{g_{o2}}{g_{o1}} + \frac{g_{m2}}{g_{o1}}}$$

$$= \frac{g_{o1}g_{o2}}{g_{o1} + g_{o2} + g_{m2}}$$

$$\therefore Y_{o\text{eff}} = \frac{g_{o1} + g_{o2} + g_{m2}}{g_{o1}g_{o2}}$$

$$= \frac{1}{g_{o2}} + \frac{1}{g_{o1}} + \frac{g_{m2}}{g_{o1}g_{o2}}$$



$$\therefore r_{o\text{eff}} = r_{o1} + r_{o2} + r_{o1} \left(\frac{g_{m2}}{g_{o2}} \right)$$

$$= r_{o1} + r_{o2} + A_{v2} r_{o1}$$

$$r_{o\text{eff}} = r_{o2} + (1 + A_{v2}) r_{o1}$$

Voltage Gain $A_{v\text{eff}}$ of the Cascode Stage Amplifier is

$$A_{v\text{eff}} = - \frac{g_{m\text{eff}}}{g_{o\text{eff}}} = - g_{m1} [r_{o2} + (1 + A_{v2}) r_{o1}]$$

$$= + A_{v2} + A_{v1} + A_{v1} A_{v2}$$

$$\approx A_{v1} \cdot A_{v2}$$

If $A_{v1} = A_{v2}$
then $A_{v\text{eff}} = A_{v1}^2$



Gain Bandwidth Product GBW of Cascode

$$= \frac{g_{m\text{eff}}}{C_{in}} \approx \frac{g_{m1}}{C_{in}} \rightarrow \underline{\text{NO CHANGE}}$$

If $M1$ & $M2$ are identical, then $g_m = g_{m1} = g_{m2}$
 $r_o = r_{o1} = r_{o2}$

Then $\text{Gain}_{\text{cascode}} \approx (\text{Gain}_{\text{single stage}})^2$

For Cascode, Gain Enhances (Boosted) but
 Bandwidth remains same.

Thus Technology Constraint of Transistor is as if BROKEN.