

In an Integrated Circuit fabrication, many films of different materials are deposited.



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These films are of either Metals, Metal-silicides, and Dielectrics like SiO_2 , Si_3N_4 .

Requirements of Deposition

- i Desired Composition, Low Contaminates
- ii Good Electrical properties of films (Desired)
- iii Mechanical Properties should also be good.
Adhesion is one such important Property

Two Major Deposition Techniques :

1. Physical Vapour Deposition (PVD)

(a) Evaporation

(b) Sputtering

2. Chemical Vapour Deposition (CVD)

a. At. Pressure CVD (APCVD)

b. Low Pressure CVD (LPCVD)

c. Plasma Enhanced CVD (PECVD)

d. Hot-Wire CVD (HWCVD)



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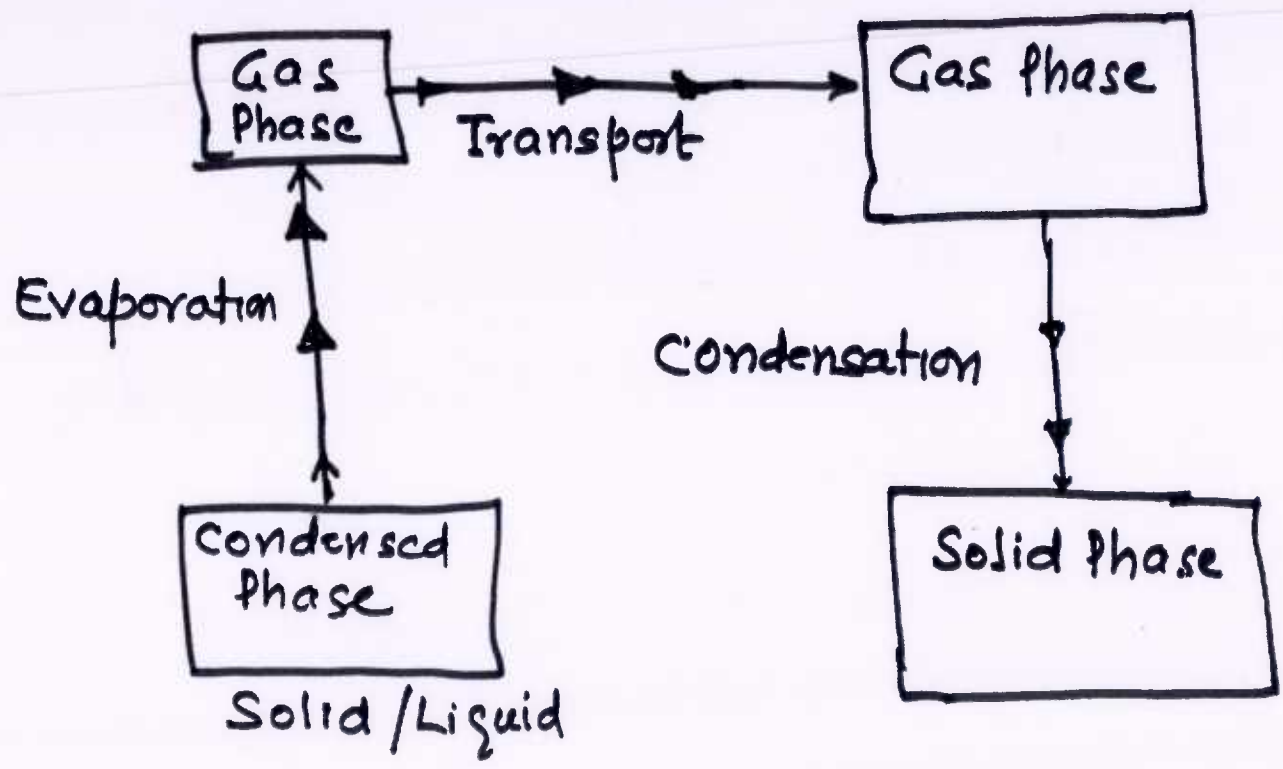
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Typical PVD process looks like
a Four Step Process



Evaporation System Requirement



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1. Vacuum :

- Need 10^{-6} torr or better vacuum for better quality films.

- Better vacuum be Ultra High Vacuum which could be around 10^{-9} torr.

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2. Heating System

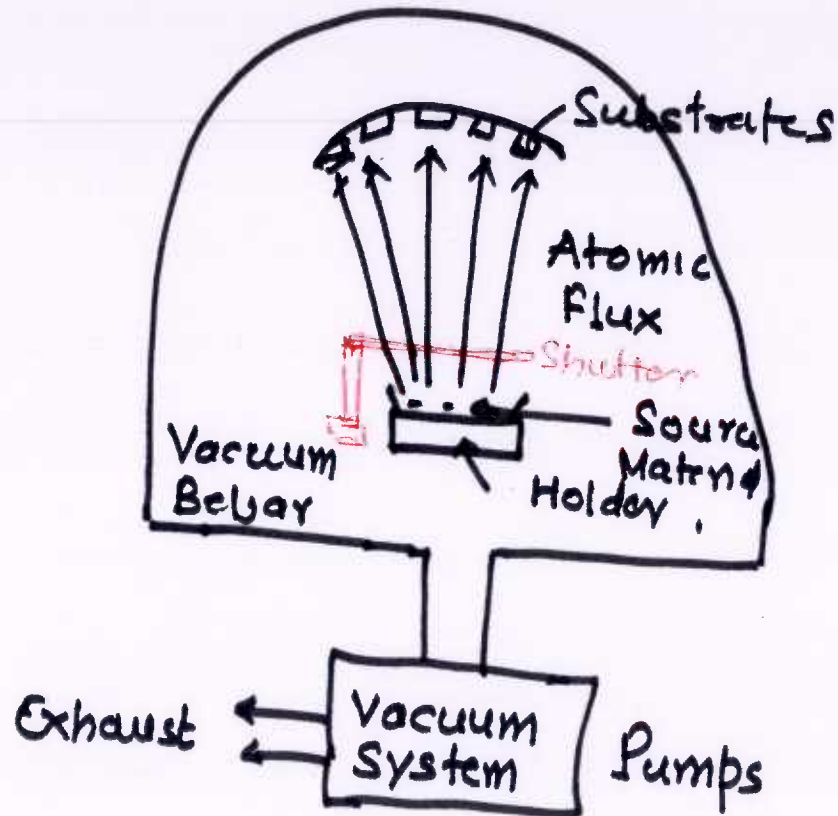
}	Thermal Heating	} 1-10 kW Power
	Electron-Beam related	

3. A Bell-Jar to keep vacuum.

4. Thickness Monitor

5. Mechanical Shutter System

Control on evaporating flux reaching substrate



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Modeling of Evaporation:

- (i) We define p^* as Partial Pressure of a gas in equilibrium with its Condensed Phase at a given Temperature T .

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Generally p^* is only function of Temperature (T).

- (ii) p is defined as ambient hydrostatic pressure acting upon evaporant in Condensed State

According to Hertz Principle, the evaporation rate is $\propto (p^* - p)$

In vacuum, p is closed to zero



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ciii) V_g and V_c are volume of evaporant in Gas Phase and Condensed Phase respectively.

(iv) If we define ΔH_e as enthalpy-change from one phase going to the, other, then

according to Clausius Clapeyron Equation

$$\frac{dp^*}{dT} \propto \frac{\Delta H_e}{T(V_g - V_c)} \approx \frac{\Delta H_e}{T V_g}$$

(Normally $V_g \gg V_c$)

By Ideal Gas Laws

$$p^* V_g = RT$$

where R is Universal Gas Constant



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Clausius - Clapeyron Equation



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$$\therefore \frac{dp^*}{p^*} = \frac{\Delta H_e}{RT^2} dT$$

$$\text{or } \ln p^* = - \frac{\Delta H_e}{RT} + c^*$$

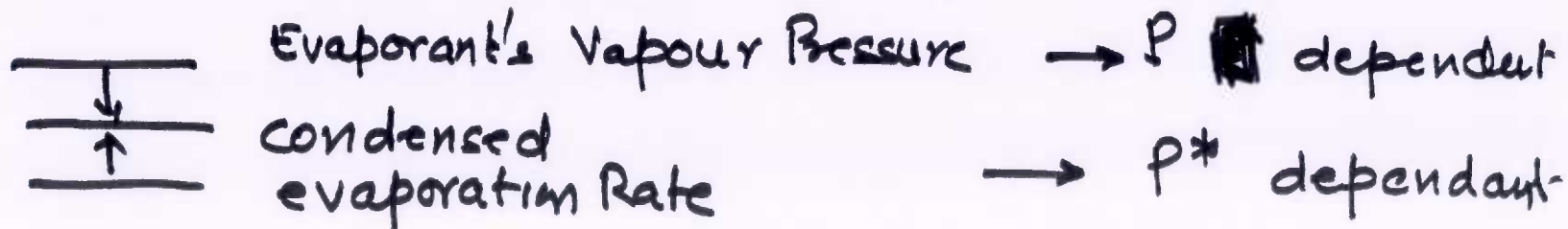
Let $c^* = \ln C_1$

$$\therefore p^* = C_1 e^{-\Delta H_e/RT}$$

Clearly p^* is only function of Temperature T

(V) Evaporation Rate R_{ev}

We have two Fluxes:



If A is cross-section area of flux coming out of evaporator, then

$$\frac{1}{A} \frac{dN_e}{dt} = \frac{1}{(2\pi m kT)^{1/2}} (P^* - P)$$

where $\frac{1}{A} \frac{dN_e}{dt}$ represents net Evaporation Rate

$$\text{or } R_{ev} = \frac{1}{A} \frac{dN_e}{dt} = \frac{1}{(2\pi m kT)^{1/2}} (P^* - P)$$

Hertz-Knudson equation for R_{ev} also takes care of return flux which is decided by α_v called Sticking Coeff for vapour molecules on the surface and thus is written as



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$$R_{ev} = \frac{1}{A} \frac{dN_e}{dt} = \alpha_v (2\pi m k T)^{-1/2} (P^* - P)$$

In vacuum, two things are affected

ci) P the pressure due to return flux

could be closed to $\rightarrow 0$ (Zero). Knudsen cell can ensure this.

Δ ci) The mean free path of evaporant atoms increases i.e.

$$\lambda = \frac{kT}{\sqrt{2} \pi \sigma^2 P}$$

Clearly better vacuum means higher mean free path.

Higher Mean Free Path means, unlikely events of collision between evaporant atoms \Rightarrow Unidirectional Flow.



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