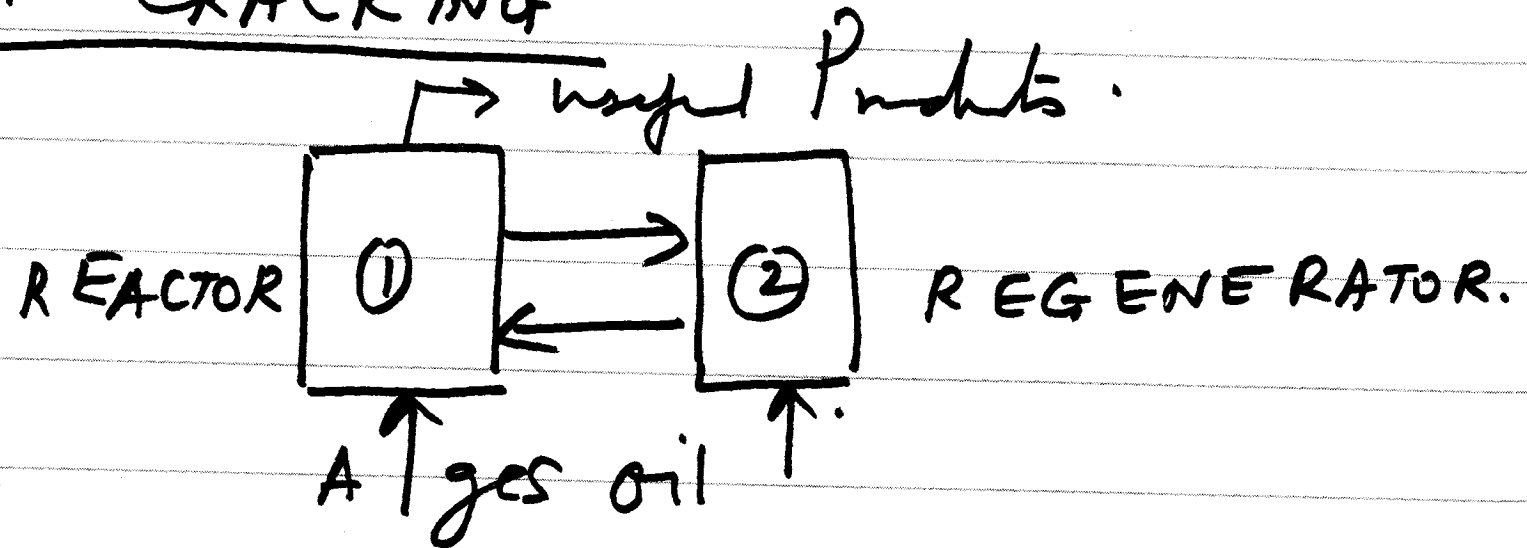


CAT CRACKING



$$r_1 = -k_1 \bar{a}_1 \checkmark$$

\bar{a}_1

$$r_2 = k_2 (1 - \bar{a}) \checkmark$$

\bar{a}_2

$$-r_A = k_r C_A \bar{a}_1$$

2

$$v_0 \bar{a}_2 - v_0 \bar{a}_1 - k_1 W_1 \bar{a}_1 = 0 \quad \text{REACTOR}$$

$$v_0 \bar{a}_1 - v_0 \bar{a}_2 + k_2 W_2 (1 - \bar{a}_2) = 0 \quad \text{REG.}$$

$$\bar{t}_1 = \frac{\bar{a}_2 - \bar{a}_1}{k_1 \bar{a}_1}$$

$$\bar{t}_2 = \frac{\bar{a}_2 - \bar{a}_1}{k_2 (1 - \bar{a}_2)}$$

$$\boxed{\bar{a}_2 - \bar{a}_1 = -\Omega}$$

3

$$\frac{\bar{t}_1}{\bar{t}_2} = \frac{\bar{a}_1}{1 - \bar{a}_2}$$

$$\bar{a}_2 - \bar{a}_1 = 0.3$$

$$k_1 = 0.5/s \text{ at } G_A = \frac{1.5g}{L}$$

$$k_2 = 0.4/s.$$

$$\frac{\bar{t}_1}{\bar{t}_2} = \left(\frac{k_2}{k_1} \right)^{1/2}$$

$$G_{A0} = g/L$$

$$k_1 \text{ at } G_A = G_{A0}(1-x) \Rightarrow 5(1-0.6) = 2g/L$$

$$\bar{t}_1 = \frac{0.3}{(0.66)(0.307)} = 1.43 s$$

④

$$\bar{t}_2 = \frac{0.3}{(0.4)(0.607)} = 1.23 \text{ s}$$

$$-r_A = \cancel{k_r} k_r C_{A0} (1-x) \bar{a}_1$$

$$= \cancel{0.4} (0.867) \cancel{(1-0.6)}$$

$$k_r C_{A0} = 0.867$$

$$k_r C_A = \left(\frac{0.867}{5} \right)^2 = 0.346 \cancel{3} / \text{s}$$

5

$$-r_A = k_r C_{A0} (1-x) \bar{a}_1$$

$$= (0.867) (1-0.6) 0.307 = 0.106$$

REACTOR

$$F_{A0} - F_A + r_A W = 0$$

$$\underbrace{F_{A0} - F_A} - \underbrace{k_r C_{A0} (1-x) \bar{a}_1}_{0.106} W_1 = 0$$

$$(0.6) 16 \text{ kg/s} - 0.106 W_1 = 0$$

①

$$W_1 = \frac{(0.6)(16)}{0.106} = 91 \text{ kg}$$

$$F_s = W_1 / \bar{t}_1 = \frac{91}{1.43} = 65 \text{ kg/s}$$

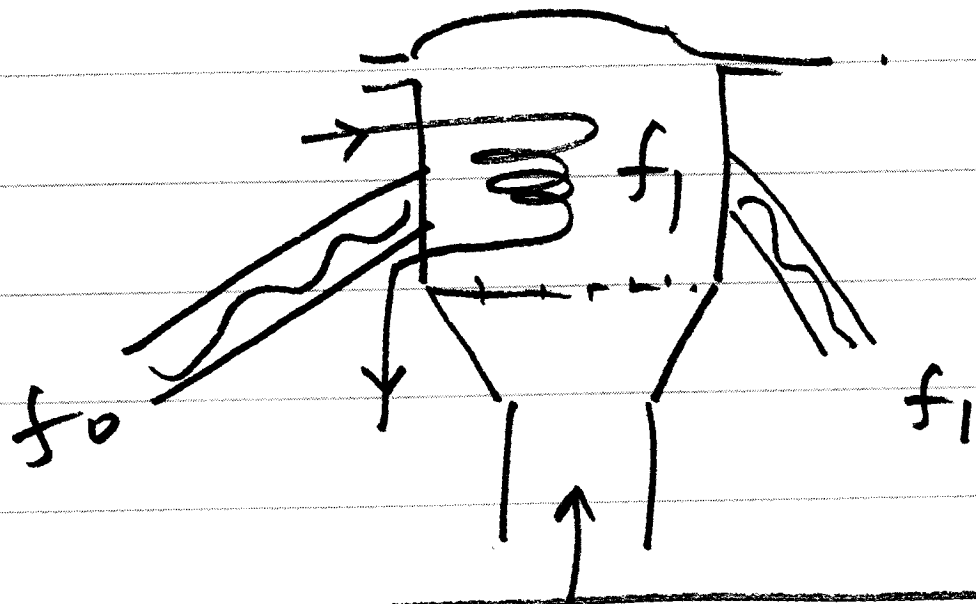
$$W_2 = (F_s) \bar{t}_2 = (65 \text{ kg/s}) 1.23 =$$

~~80 kg~~
80 kg

$F_{A0} = 16 \text{ kg/s}$
$F_s = 65 \text{ kg/s}$

7

Q7 PARTICLE SIZE DISTRIBUTION FLUID BED COMBUSTOR.



REACTION CONTROL

$$f_0 = \delta(s-1).$$

$$s = r/R = 1$$

$$f_0 - f_1 = \frac{d}{ds} (f, r, \bar{t}_1) = 0.$$

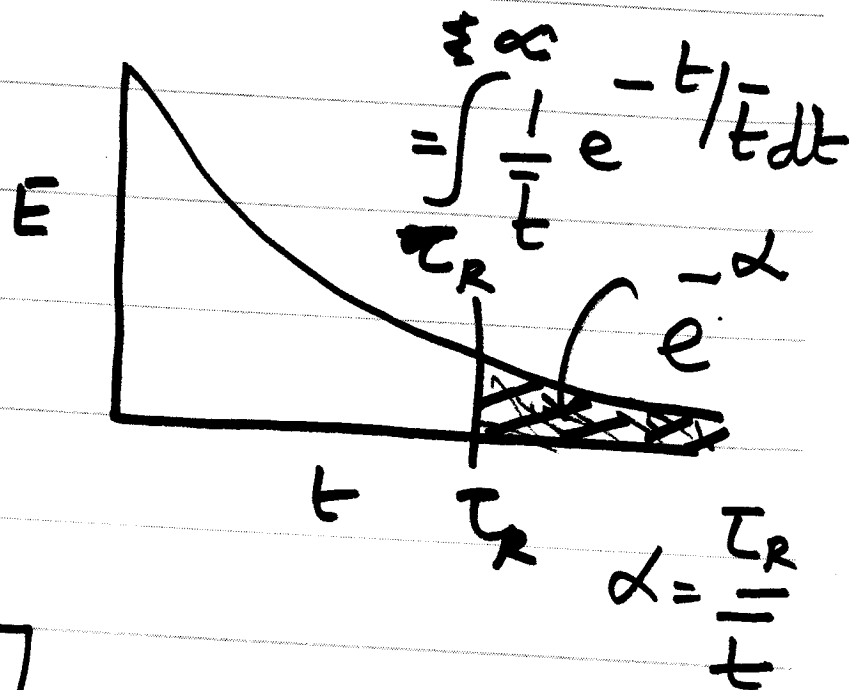
8

$$f_1 = g_1(s) + K_0 \delta(s-0)$$

$$1 - \frac{\gamma}{R} = \frac{t}{\tau_R}$$

Reaction Contr. Ω .

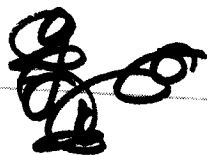
$$\frac{ds}{dt} = 1 - s = \frac{t}{\tau_R}$$
$$r_1 = \left(\frac{ds}{dt} \right) = -\frac{1}{\tau_R}$$



$$\int f_1 ds = 1 = \int_0^{\infty} g_1 ds + K_0$$

$$1 - K_0 = \int g_1 ds$$

9



$$f_0 - f_1 - \frac{d}{ds} (f, r, \bar{t}_1) = 0 \quad \times$$

$$g_1 + \frac{d}{ds} (g, r, \bar{t}_1) = 0 \quad \checkmark$$

$$r_1 = -\frac{1}{\tau_R}$$

$$\ln\left(\frac{g, r, \bar{t}_1}{\varphi}\right) = \tau_R / \bar{t}_1 \quad \checkmark$$

$$\alpha = \frac{\tau_R}{\bar{t}_1}$$

$$g, r, \bar{t}_1 = \varphi e^{\alpha s}$$

10

B.C

Balana $(s-ds)$ & s .

$$\lim_{s \rightarrow 0} \quad ds \rightarrow 0$$

$$1/p - 0/p + Gen = 0$$

$$\lim_{s \rightarrow 0} \int ds \quad v_0 \delta(s-1) ds \quad v_0 \left[\cancel{g_1} + K_0 \delta(s-0) \right] ds$$

$$\lim_{ds \rightarrow 0} \quad + W_1 r_1 \cancel{(s-ds)} g_1(s-ds) - W_1 r_{\#}(s) g_1(s) = 0$$

$$-v_0 K_0 - (W_1 r_1 g_1)_0 = 0$$

$$\boxed{(g_1 r_1 \bar{t}_1)_0 = -K_0}$$

②

$$g_1(0) = \left[-\frac{1}{\tau_R} \bar{E}_1 \right] = -K_0$$

$$g_1(0) = \frac{\tau_R}{T} K_0 =$$

$$\frac{1}{\tau_R} g_1(0) = \alpha e^{-\alpha}$$

(12)

$$g, r, \bar{t}_1 = \overset{\downarrow}{Q} e^{\alpha s}.$$

$$g, (0) = \alpha e^{-\alpha}$$

$$Q = -e^{-\alpha}.$$

$$g, (s) = \alpha e^{\alpha(s-1)}$$

$$f_1 = \alpha e^{\alpha(s-1)} + K_0 \delta(s-0)$$

$$f_1 = \alpha e^{\alpha(s-1)} + e^{-\alpha} \delta(s-0)$$

Mean Conversion at the exit.

$$1 - X_B = \left(\frac{r}{R}\right)^3$$

$$\overline{1 - X_B} = \frac{\int_0^R \frac{4}{3} \pi r^3 f(r) dr \rho_B}{\frac{4}{3} \pi R^3 \rho_B}$$

(14)

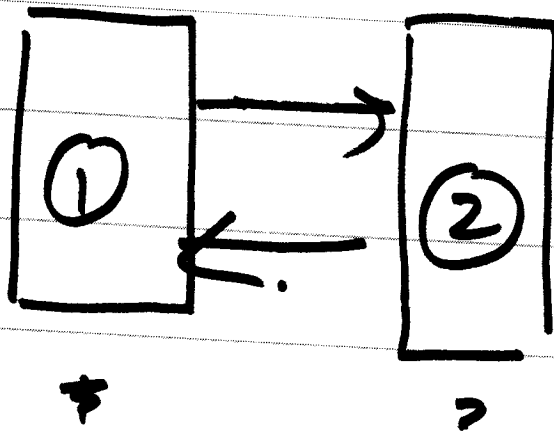
$$\overline{1-X_B} = \int_0^1 s^3 f(s) ds$$

$$\overline{1-X_B} = \int_0^1 \left[s^3 \left\{ g_1(s) ds + k_0 \delta(s-0) \right\} \right] ds$$

$$\overline{1-X_B} = \int_0^1 s^3 g_1(s) ds = \int_0^1 s^3 \left\{ \alpha e^{\alpha(s-1)} ds \right\}$$

$$\overline{1-X_B} = 1 - \frac{3}{\alpha} + \frac{6}{\alpha^2} - \frac{6}{\alpha^3} + \frac{6e^{-\alpha}}{\alpha^3}$$

(15)

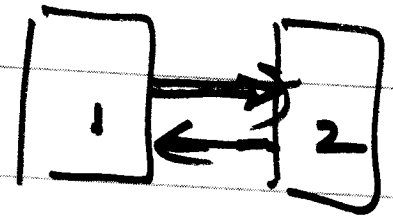


$$r_1 = -k_1 \text{ (s)}$$

$$r_2 = k_2$$

Find f_1 and f_2

PBE
Reactor.



$$f_1 = g_1 + k_0 \delta(s-0) \quad (1)$$

$$f_2 = g_2 + k_1 \delta(s-1) \quad (2)$$

$$g_1 = -k_1 s$$

$$g_2 = +k_2$$

(17)

PBE:

Reacts

\bar{g}

$$g_2 - g_1 - \frac{d}{ds} (g_1 r_1 \bar{t}_1) = 0$$

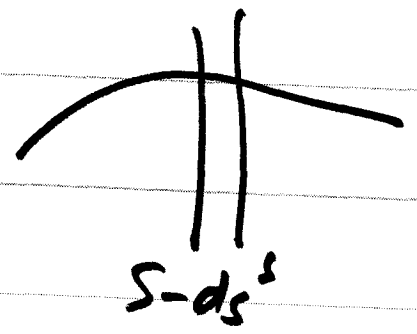
Leg

$$g_1 - g_2 - \frac{d}{ds} (g_2 r_2 \bar{t}_2) = 0$$

$$\frac{d}{ds} (g_1 r_1 \bar{t}_1 + g_2 r_2 \bar{t}_2) = 0$$

$$g_1 r_1 \bar{t}_1 + g_2 r_2 \bar{t}_2 = \text{Constant}$$

Reater



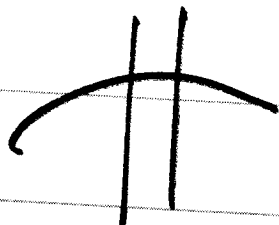
$$\begin{aligned}
& \frac{1}{\rho} - \frac{0}{\rho} + G = 0 \\
& \int_0^s [g_2 ds + L \delta(s-1)] ds \\
& - \int_0^s g_1 ds \\
& + W g_1 (s-ds) r_1 (s-ds) \\
& - W g_1 (s) r_1 (s) = 0
\end{aligned}$$

$$(g_1 r_1 \bar{t}_1)_0 = 0$$

Let $s \rightarrow 0$
 $ds \rightarrow 0$

$$\text{At } s \rightarrow 1 \quad ds \rightarrow 0$$

Leader



$s \quad s+ds.$

$$\frac{1}{\rho} \frac{d\rho}{ds} + g_{en} = 0$$

$$v_0 \left[\cancel{g_1 ds} + L_1 \delta(s-1) ds \right]$$

$$\left(g_1, r, \bar{h} \right)_1 = -L_1$$

At

$$- \cancel{v_0 g_1 ds}$$

$s \rightarrow 1$

$ds \rightarrow 0$

$$+ W \rho_1(s) g_1(s) - W \rho_1(\cancel{s}) g_1(\cancel{s+ds})$$

$$= 0$$

Rayonlar

$$[s-ds, s]$$

$$\text{Let } s \rightarrow 0 \quad ds \rightarrow 0$$

$$v_0 \cancel{g_1 ds} - v_0 [g_2 + L, \cancel{\sigma(s-1)}] ds$$

$$+ W_2 g_2 (s - \cancel{ds}) r_2 (s - ds)$$

$$- W_2 g_2 (s) r_2(s) = 0$$

$$(g_2 r_2 \bar{t}_2)_0 = 0$$

$$(g_2 r_2 \bar{t}_2)_1 = L_1$$

(21)

$$(g_1 r_1 \bar{t}_1)_0 = 0 \quad (g_2 r_2 \bar{t}_2)_0$$

So Cond of Intg = 0.

$$g_1 r_1 \bar{t}_1 + g_2 r_2 \bar{t}_2 = 0$$

$$g_2 = \frac{-g_1 r_1 \bar{t}_1}{r_2 \bar{t}_2}$$

Recht

(22)

$$-g, r, \bar{t}_1 - \frac{d g, r, \bar{t}_1}{ds} = 0$$

$$\frac{d g, r, \bar{t}_1}{ds} = -g, r, \bar{t}_1 \left[\frac{1}{r_1 \bar{t}_1} + \frac{1}{r_2 \bar{t}_2} \right].$$

$$r_1 = -k_1 s$$

$$r_2 = +k_2 s$$

23

$$\ln \left[\frac{g, r, \bar{t}_1}{\varphi} \right] - \alpha \ln s = -\beta s$$

$$\ln \frac{g, r, \bar{t}_1}{\varphi} = \ln s^\alpha = -\beta s$$

$$g, r, \bar{t}_1 = \varphi s^\alpha \exp(-\beta s)$$

$$g_1 = -\varphi \alpha s^{\alpha-1} \exp(-\beta s)$$

$$g_2 = -\varphi \beta s^\alpha \exp(-\beta s).$$

25

$$t = \tau_r (1 - r_c/r) + \tau_p \left[1 - 3 \frac{r_c^2}{R^2} + 2 \frac{r_c^3}{R^3} \right].$$

$$\frac{\tau_{R1} (4\text{mm})}{\tau_{R2} (12\text{mm})} = \frac{4}{12} = \frac{1}{3}$$

$$\frac{\tau_{D1} (4\text{mm})}{\tau_{D2} (12\text{mm})} = \left(\frac{4^2}{12^2} \right) = \frac{16}{144} = \frac{1}{9}$$

26

$$1 - X_B = 0.5$$

$$0.5 = 1 - X_B = \left(\frac{r_c}{R} \right)^3$$

$$\left(\frac{r}{R} \right) = (1 - 0.5)^{1/3} = 0.79$$

24

GAS SOLID REACTIONS

Data

Neglect Film Diff Control.

d_p

4 MM

12 MM

T

550

590

Time for

15 MIN

2 Hrs

50%.

CONV

Time for 98% CONVERSION OF 3MM
particle

4MM Particles

(550C) $0.25 = \tau_{R1} (1 - 0.8) + \tau_{D1} (1 - 3(0.8)^2 + 2(0.8)^3)$

12MM Particles

(590C)

$2 = \tau_{R2} (1 - 0.8) + \tau_{D2} [1 - 3(0.8)^2 + 2(0.8)^3]$

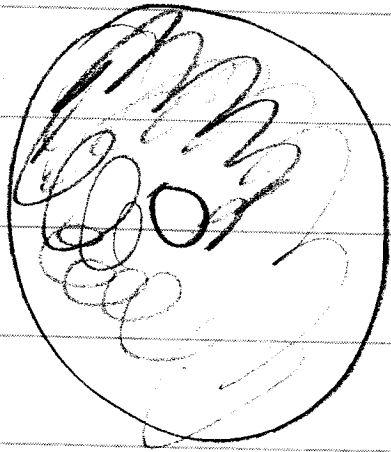
$\tau_{D1} = \frac{0.35 \text{ hrs}}{2} = 2.25$

$\tau_{D2} = \frac{2.25 \text{ hrs}}{18} = 0.125 \text{ hrs}$

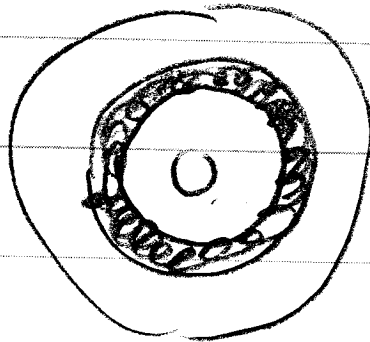
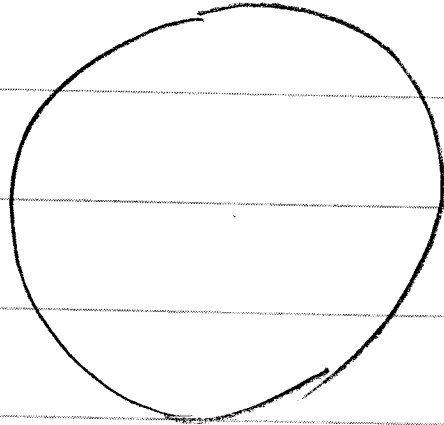
$\tau_{R1} = \frac{0.35 \text{ hr}}{1.7} = 0.208 \text{ hr}$

$\tau_{R2} = 0.624 \text{ hrs.}$

Ree



Lo₁



$$\frac{h}{3} (4\pi r_c^2)$$

